

A Multi-Slotted Wide Microstrip Patch Antenna for Dual Frequency

Ram Singh Kushwaha¹, D.K.Srivastava², J.P.Saini³

¹Department of Electronics and Communication Engineering, BIET Jhansi, INDIA

²Department of Electronics and Communication Engineering, BIET Jhansi, INDIA

³Madan Mohan Malviya College of Engineering, Gorakhpur, INDIA

Abstract— This paper presents a compact, wideband microstrip patch antenna with a E-shape slot for dual frequency. The proposed antenna operates at 1.95 GHz and 2.93 GHz bands. The antenna size is very compact (40 mm x 60 mm x 1.6 mm) and is fed from a 50 Ω microstrip line. Using IE3D software package of Zeland, according to the set size, the antenna is simulated. The computer simulation results show that the antenna can realize wide band characters. The two operating bands exhibit broad impedance bandwidths (VSWR ≤ 2) of about 25% and 15%.

Keywords— Microstrip antenna, E-shape slot, dual frequency, microstrip line, IE3D.

1. INTRODUCTION

The rapid development of wireless communication technology has increased the demand for compact microstrip antennas with high gain and wideband operating frequencies. Microstrip patch antennas are very advantageous because of their low cost, low profile, light weight and simple realization process. However, the general microstrip patch antennas have some disadvantages such as narrow bandwidth etc. Enhancement of the performance to meet the demanding bandwidth is necessary [1]. There are numerous and well-known methods to increase the bandwidth of antennas, including increase of the substrate thickness, the use of a low dielectric substrate, slotted patch antenna, the use of various impedance matching and feeding techniques [2-17].

This paper presents a new E-shaped slot loaded patch antenna that is investigating for enhancing the impedance bandwidth. By choosing the suitable slot shape, selecting a proper feed and tuning their dimensions, a large operating bandwidth is obtained. The design employs 50 Ω microstrip line feeding. The antenna is simulated using IE3D software package of Zealand. The results show that the impedance bandwidth has achieved a good match.

II. ANTENNA GEOMETRY

The dielectric constant of the substrate is closely related to the size and the bandwidth of the microstrip antenna. Low dielectric constant of the substrate produces larger bandwidth, while the high dielectric constant of the substrate results in smaller size of antenna. A trade-off relationship exists between antenna size and bandwidth [18].

The resonant frequency of microstrip antenna and the size of the radiation patch can be similar to the following formulas [19].

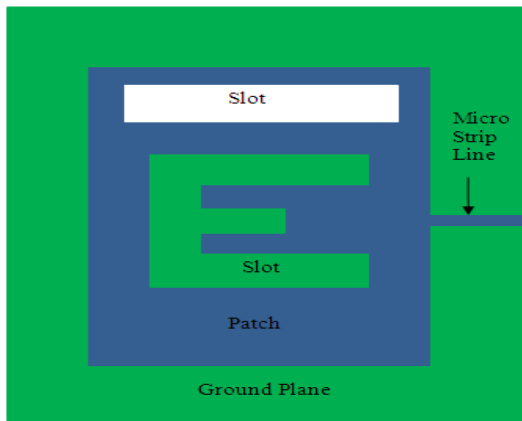
$$f \cong \frac{c}{2L\sqrt{\epsilon_r}} \quad (1)$$

$$W = \frac{2}{f_r} \left(\frac{\epsilon_r + 1}{2} \right)^{\frac{1}{2}} \quad (2)$$

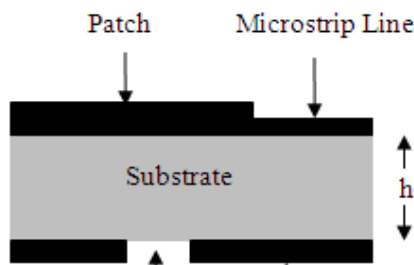
$$L = \frac{c}{2f_r\sqrt{\epsilon_r}} - 2\Delta l \quad (3)$$

Where f is the resonant frequency of the antenna, c is the free space velocity of the light, L is the actual length of the current, ϵ_r is the effective dielectric constant of the substrate and Δl is the length of equivalent radiation gap.

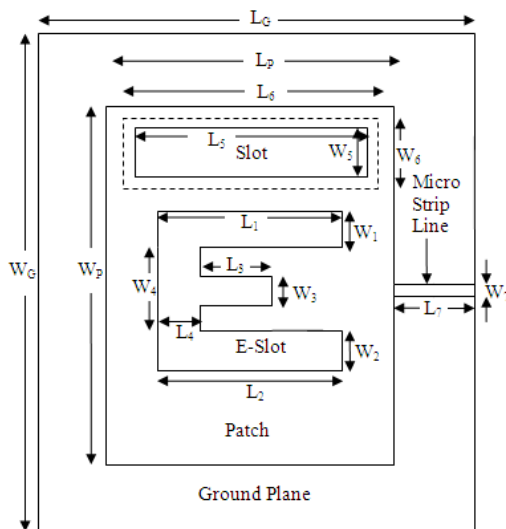
The geometries of the E-shaped slot antenna are shown in figure 1. The antenna is built on a glass epoxy substrate with dielectric constant 4.2 and height h of 1.6 mm. A substrate of low dielectric constant is selected to obtain a compact radiating structure that meets the demanding bandwidth specification. For the given design the slot and the feeding line are printed on the same side of the dielectric substrate. The geometry of the top view and side view of the proposed antenna is shown in figure 1 (a) and (b) respectively. The dimensions of the slotted patch are shown in figure (c). Here L_G and W_G represent the length and width of the ground plane which is finite whereas L_P and W_P are those of the patch. The lengths of the horizontal arms of the E-shape slot are defined by L_1 , L_2 and L_3 where as W_1 , W_2 and W_3 define the widths. The length and width of the vertical arm are defined by L_4 and W_4 respectively. The patch is also loaded with a horizontal slot at center coordinates (20, 50). The length and width of the slot are shown by L_5 and W_5 respectively. An additional horizontal slot is cut on the ground plane, whose length and width are shown by L_6 and W_6 respectively. The patch is fed by a 50 Ω microstrip line whose length and width are defined by L_7 and W_7 respectively. The use of microstrip line feeding technique provides the bandwidth enhancement. Table 1 shows the optimized design parameters for the proposed antenna.



(a) Top view of the antenna.



(b) Side view of the antenna.



(c) Dimensions of the antenna.

Fig.1. Geometry of the proposed antenna.

Table 1. The proposed patch antenna design parameters.

| Parameter | Value [mm] | Parameter | Value [mm] |
|-----------|------------|-----------|------------|
| W_G | 60 | L_3 | 10 |
| L_G | 40 | W_4 | 10 |
| W_P | 50 | L_4 | 5 |
| L_P | 30 | W_5 | 8 |
| W_1 | 5 | L_5 | 25 |
| L_1 | 20 | W_6 | 9 |
| W_2 | 5 | L_6 | 30 |
| L_2 | 20 | W_7 | 2 |
| W_3 | 5 | L_7 | 5 |

Reducing the size of the antenna is one of the key factors to miniaturize the wireless communication devices. However, reducing the antenna size will usually reduce its impedance bandwidth as well. Therefore designing a small antenna operating with a wide impedance bandwidth which satisfies future generation wireless application is a challenging work, especially having stable radiation patterns across the operating frequency band [20-21]. In this paper microstrip line feeding, slots on the patch as well as on ground plane provide the wide bandwidth and gain enhancement.

III. RESULTS AND DISCUSSIONS

The proposed antenna was simulated and optimized by IE3D software package of Zealand. This was used to calculate the return loss, impedance bandwidth and radiation pattern.

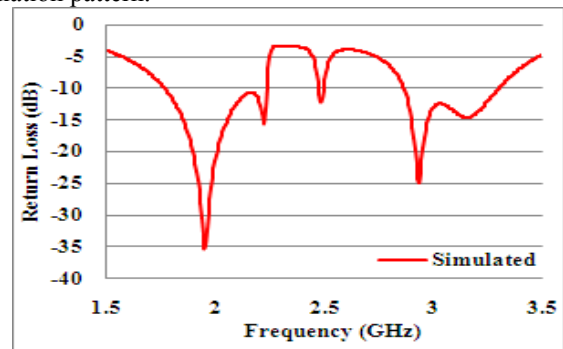
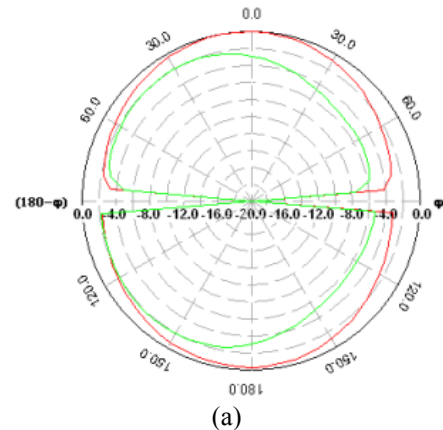
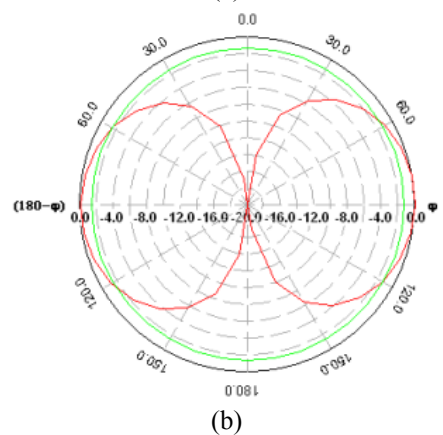


Fig.2. Simulated return loss of the proposed antenna.



(a)



(b)

Fig.3. Radiation pattern of the proposed antenna. (a) Elevation and (b) Azimuth.

The simulated -10 dB return loss of the proposed antenna is shown in the figure 2. The simulated result shows that the

first band resonant frequency locates at about 1.95 GHz with the -10 dB impedance bandwidth from about 1.765 GHz to 2.238 GHz. The second band resonant frequency locates at about 2.93 GHz with the impedance bandwidth from about 2.865 GHz to 3.303 GHz. The -10 dB return loss impedance bandwidths for first and second band are 25% and 15% respectively. The simulated radiation patterns of the elevation and azimuth of the proposed antenna are shown in figure 3. It can be observed that the proposed antenna have the same radiation patterns over the entire frequency band.

IV. CONCLUSION

A novel compact dual-band slot microstrip antenna for 1.76/3.30 GHz is presented. The proposed antenna has a compact size of (40 mm x 60 mm x 1.6 mm) and it can effectively cover the AMPS, GSM and WLAN applications. Good antenna performance and impedance matching can be realized by adjusting the length and width of microstrip line. The two operating bands exhibit broad impedance bandwidths ($VSWR \leq 2$) of about 25% and 15%. It can be concluded from the results that the designed antenna has satisfactory performance and hence can be used for indoor wireless applications.

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Biographical notes

Mr. Ram Singh Kushwaha is a lecturer in the Department of Electronics and Communication Engineering, Bundelkhand Institute of Engineering and Technology Jhansi, India. He has about 7 years of experience in teaching and research work.

Dr. D.K.Srivastava is a Reader in the Department of Electronics and Communication Engineering, Bundelkhand Institute of Engineering and Technology Jhansi, India. He has more than 14 years of experience in teaching, research and administrative work. His current area of research includes Microwaves and Optical communication. He has published around five papers in referred international journals. He has also presented more than twenty research articles in national and international conferences. He is Member IEEE.

Dr. J. P. Saini is a Professor in the Department of Electronics and Communication Engineering, Bundelkhand Institute of Engineering and Technology Jhansi, India. He has more than 25 years of experience in teaching, research and administrative work. His current area of research includes Multi-criteria Decision-Making, Neural Networks, and Optical and photonic waveguides. He has published more than twenty papers in referred international journals. He has also presented nearly fifty research articles in national and international conferences. He is currently working as a Principal of Madan Mohan Malviya Engineering College, Gorakhpur, India on deputation. He is life Member IETE and ISTE and Member IEEE (Ex.).